LiDAR Remote Sensing Data Collection:
Columbia River Survey
Delivery 3

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1. Overview

Watershed Sciences, Inc. (WS) is currently collecting Light Detection and Ranging (LiDAR) data of the Columbia River in Oregon, Washington, Idaho, and Montana. The requested AOI area for this delivery was 102,837 acres. The area was expanded to include a 100 m buffer to ensure complete coverage and adequate point densities around survey area boundaries, resulting in 115,200 acres of delivered data. LiDAR data for Delivery 3 was collected between November 25th, 2009 and February 10th, 2010 (**Figure 1**). This area includes portions of the Columbia River from Priest Rapids Dam to Chief Joseph Dam. This report contains maps and information specific to Delivery 3, but has been appended to the previous delivered reports to generate a cumulative data summary for UTM Zone 10 and 11. Accuracy and density data will continue to be updated as additional data is processed.

Figure 1. Columbia River survey delivery status overview.

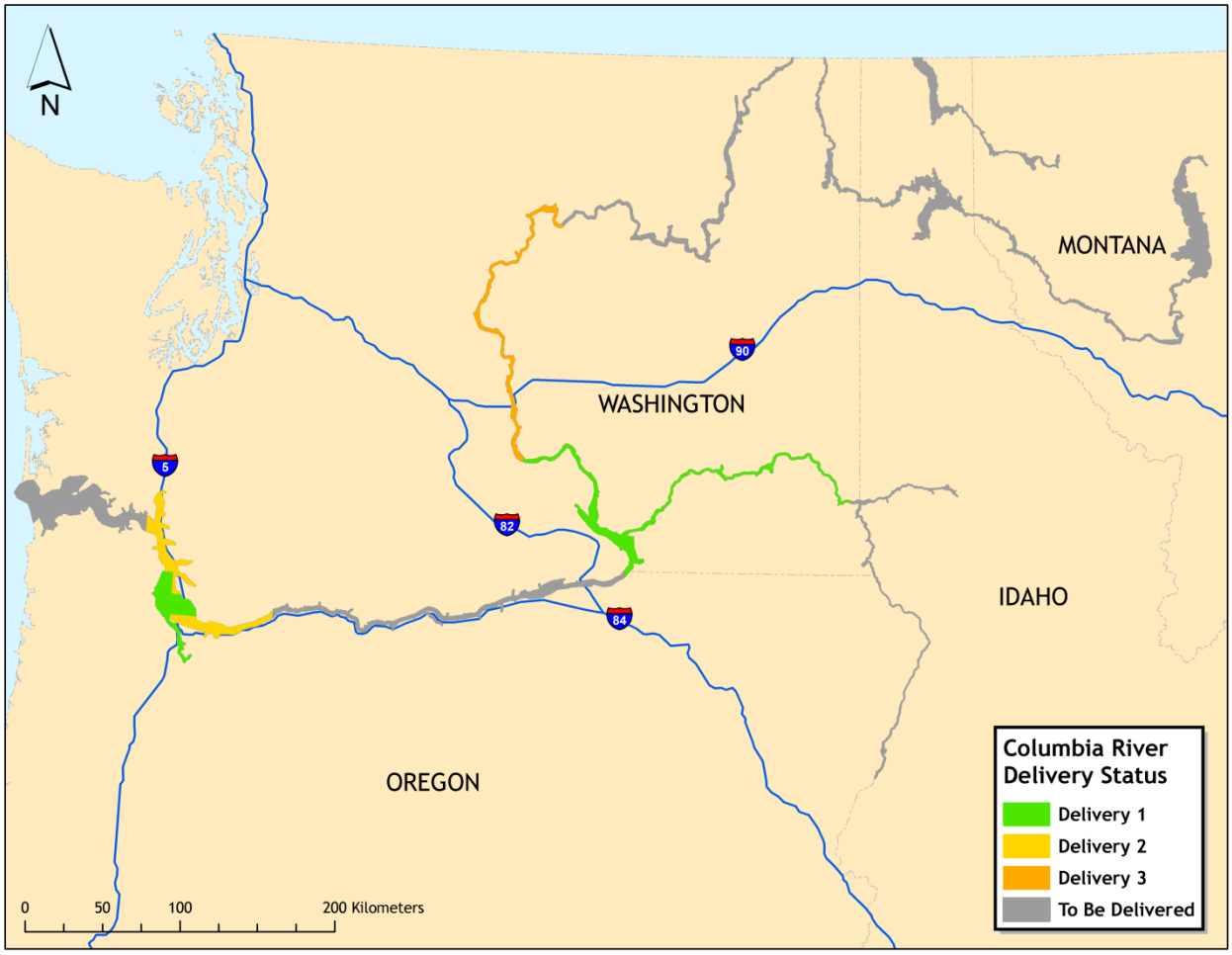


Table 1. Columbia River, UTM Zone 10 and 11 LiDAR deliveries to date.

UTM 10 Delivery	Date	Total Acres Flown	AOI Acres
1	April 15, 2010	129,000	125,409
2	May 13, 2010	191,071	181,694
UTM 11 Delivery	**Date**	**Total Acres Flown**	**AOI Acres**
1	April 15, 2010	206,500	187,764
3	May 20, 2010	115,200	102,837

2. Acquisition

2.1 Airborne Survey – Instrumentation and Methods

The LiDAR survey uses Leica ALS50 Phase II and ALS60 laser systems. For the Columbia River survey sites, the sensor scan angle was ±14° from nadir[1] with a pulse rate designed to yield an average native density (number of pulses emitted by the laser system) of ≥ 8 points per square meter over terrestrial surfaces. It is not uncommon for some types of surfaces (e.g. dense vegetation or water) to return fewer pulses than the laser originally emitted. These discrepancies between 'native' and 'delivered' density will vary depending on terrain, land cover and the prevalence of water bodies.

The Cessna Caravan is a stable platform, ideal for flying slow and low for high density projects. The Leica ALS60 sensor head installed in the Caravan is shown on the left.

[1] Nadir refers to the perpendicular vector to the ground directly below the aircraft. Nadir is commonly used to measure the angle from the vector and is referred to a "degrees from nadir".

All areas were surveyed with an opposing flight line side-lap of ≥60% (≥100% overlap) to reduce laser shadowing and increase surface laser painting. The Leica laser systems allow up to four range measurements (returns) per pulse, and all discernable laser returns were processed for the output dataset.

To accurately solve for laser point position (geographic coordinates x, y, z), the positional coordinates of the airborne sensor and the attitude of the aircraft were recorded continuously throughout the LiDAR data collection mission. Aircraft position was measured twice per second (2 Hz) by an onboard differential GPS unit. Aircraft attitude was measured 200 times per second (200 Hz) as pitch, roll and yaw (heading) from an onboard inertial measurement unit (IMU). To allow for post-processing correction and calibration, aircraft/sensor position and attitude data are indexed by GPS time.

2.2 Ground Survey – Instrumentation and Methods

The following ground survey data were collected to enable the geo-spatial correction of the aircraft positional coordinate data collected throughout the flight, and to allow for quality assurance checks on final LiDAR data products.

Trimble GPS survey equipment

2.2.1 Survey Control

Simultaneous with the airborne data collection mission, we conducted multiple static (1 Hz recording frequency) ground surveys over monuments with known coordinates (**Table 2)**. Survey control monuments were occupied by a Trimble GPS base station for an initial period of at least eight hours. All monuments were occupied during a subsequent second session with an observation period of at least four hours. Additional occupations were conducted as necessary. GPS measurements were made with dual frequency L1-L2 receivers with carrier-phase correction.

Watershed Sciences established monuments using aluminum survey caps provided by the Army Core of Engineers. Monuments were placed using 5/8" by 30" rebar covered with a 2" top aluminum cap stamped "U.S. Army C. of E. Portland Dist.". In addition, monuments were stamped in the field with the year and monument ID number.

As an initial check, the NGS on-line positioning user service (OPUS), was used to generate a corrected position for all base station observations. OPUS provides a measurement solution based on three surrounding continuously operating reference stations (CORS). OPUS output includes a solution report with positional accuracy confidence intervals for adjusted coordinates and elevations. The solution report is one component in assessing the quality of the OPUS GPS measurement solutions. Statistical checks of GPS base station positions and repeat control observations include the OPUS solution extended output report. In addition,

the standard deviation, kurtosis, and skew of the measurement distribution for each base station occupation were compared. Longitude, latitude, and elevation distributions were separated, and graphic distributions of the positions were plotted for consistency.

Indexed by time, these GPS data are used to correct the continuous onboard measurements of aircraft position recorded throughout the mission. Control monuments were located within 13 nautical miles of the survey area(s).

David Evans and Associates (DEA) provided the official quality assurance and control checks of all monuments in the Columbia River project. DEA provided official coordinates for each monument through the OPUS online datasheet publication tool located on the USGS website. All monuments established by Watershed Sciences were published and made publicly available by DEA on the OPUS online datasheet website.

Table 2. DEA Certified Survey Control coordinates for Columbia Survey, UTM Zones 10 and 11.

Base Station ID	Datum: NAD83 (CORS91)		GRS80
	Latitude	Longitude	Ellipsoid Z (m)
1001-08	46 30 08.41845	116 25 47.09674	418.636
1001-09	46 29 22.56715	116 36 33.78201	660.133
1001-10	46 26 48.57603	116 49 22.85152	242.284
1001-11	46 25 37.24177	116 59 37.84839	209.652
1001-12	46 25 28.18211	117 02 53.46329	217.827
1001-14	46 31 44.00815	117 17 42.94605	806.850
1001-15	46 09 54.03848	117 05 33.99476	976.569
1001-16	46 17 49.31958	117 02 40.71052	630.834
1001-17	46 37 03.17427	117 24 34.40296	712.061
1001-18	46 33 18.67563	118 02 38.51866	431.741
1001-19	46 33 41.76252	117 53 55.49260	401.263
1001-25	46 15 24.33297	119 06 44.28009	99.580
1001-26	46 04 58.38580	118 54 08.97172	95.403
1001-27	46 32 46.94113	118 32 25.89957	226.994
1001-29	45 56 24.58774	119 18 39.87547	74.982
1001-30	45 53 42.93966	119 30 34.66550	68.346
1001-31	46 19 13.63660	118 45 33.52349	144.348
1001-32	46 26 46.23824	119 14 59.85302	171.385
1001-33	46 35 03.15569	119 17 48.43776	264.490
1001-34	46 42 39.57396	119 57 4.04702	132.138
1001-35	46 54 34.61741	119 56 52.68153	245.488
1001-36	46 38 32.50509	119 44 38.56542	107.820
1001-37	47 13 44.45729	120 00 43.49174	257.111
1001-38	47 31 01.69420	120 17 43.85407	205.565
1001-39	47 43 16.43447	120 12 05.54247	279.649

Base Station ID	Datum: NAD83 (CORS91)		GRS80
	Latitude	Longitude	Ellipsoid Z (m)
1001-40	47 39 26.74450	120 12 51.23748	201.906
1001-41	47 52 34.16577	119 55 30.35976	359.688
1001-42	48 39 42.07551	117 23 30.60182	622.831
1001-43	48 51 35.80844	117 22 12.13786	626.782
1001-44	48 20 17.00708	117 17 38.10570	609.769
1001-49	46 9 55.00289	123 8 46.34524	-15.179
1001-50	45 40 13.04470	122 45 28.31955	-14.801
1001-51	45 32 52.95203	122 24 43.61968	-13.054
1001-52	45 41 51.83170	122 44 01.68053	-14.218
1001-53	45 35 59.70785	122 37 05.21499	-9.878
1001-54	45 27 24.11542	122 33 34.92190	180.294
1001-55	45 53 58.62984	122 47 51.37721	-13.395
1001-56	45 51 15.81785	122 42 09.46615	52.600
1001-57	46 02 26.42978	122 52 01.38185	-14.215
1001-58	46 06 32.94925	122 53 01.76774	-13.830
1001-59	47 54 8.17174	118 20 3.21717	391.202
1001-60	48 11 09.36643	117 01 49.51668	610.614
1001-61	48 09 44.09840	116 45 16.23674	612.942
1001-62	48 07 48.72498	1119 18 57.73562	348.9
1001-63	48 01 58.81542	118 57 40.44029	313.960
1001-64	48 07 07.96833	118 13 10.22410	462.187
1001-65	47 55 43.85009	118 41 20.44431	376.281
1001-66	47 52 22.12511	118 19 29.21404	543.651
1001-67	48 1 3 2.65643	119 34 9.57665	313.446
1001-68	45 42 41.45706	121 46 39.21052	13.726
1001-69	45 36 9.27592	122 2 37.57775	0.213
1001-70	45 54 49.89395	122 48 12.52961	-13.482
1001-71	46 10 44.41058	123 22 37.98798	-16.494
1001-72	46 14 15.72283	123 23 47.41726	-17.845
1001-73	46 21 4.74602	123 36 24.40426	-16.407
1001-74	46 21 11.60493	123 48 45.17108	-10.855
1001-75	46 10 23.59050	123 49 53.71396	-18.455
1001-76	47 52 21.92655	118 19 29.68489	543.446
1001-77	48 5 40.67804	118 13 22.57867	444.412
1001-78	48 15 21.98771	118 8 1.18818	379.948
1001-79	48 26 26.39590	118 10 13.95491	521.192
1001-80	45 42 49.27087	121 30 39.83750	6.518
1001-81	45 40 29.62697	121 15 50.33348	11.636

Base Station ID	Datum: NAD83 (CORS91)		GRS80
	Latitude	Longitude	Ellipsoid Z (m)
1001-82	45 38 19.36274	120 58 1.24916	207.468
1001-83	45 43 47.54806	120 39 4.19711	75.572
1001-84	45 42 04.13225	120 20 40.20502	150.893
1001-85	45 47 5.76650	120 2 18.05977	109.676
1001-86	45 50 33.55651	119 42 34.81642	65.288
1001-87	46 11 28.87024	123 45 29.15267	-1.992
1001-88	46 12 49.68408	123 32 29.63952	-21.070
1001-89	46 12 49.74475	123 32 29.55793	-21.065
1001-90	46 9 11.71508	123 52 41.61185	-19.967
1001-91	46 11 48.84319	118 58 46.57016	99.304
1001-92	48 11 13.44331	116 26 13.31352	614.124
1001-93	48 7 22.89091	116 9 43.76431	617.351
1001-94	48 10 32.72797	116 13 56.37429	614.024
1001-96	48 19 22.29244	116 26 54.84914	626.666
1001-97	48 13 57.90906	116 31 44.49023	618.700
1001-98	48 51 9.21891	117 53 28.28579	466.498
1001-99	48 54 44.63988	117 47 25.87213	396.158
1001-100	48 34 12.52866	118 6 49.31299	376.733
1001-101	48 43 2.83910	118 1 34.25317	392.520
1001-102	45 33 50.44237	122 13 19.83236	159.743
1001-105	48 2 36.45812	116 37 55.66404	684.064
1001-106	48 43 14.07357	116 18 37.83010	681.977
92H-01-12	45 38 7.82857	120 54 48.13633	31.328
PID_UNK	48 18 13.13079	116 33 21.41876	631.891
PID_DH8973	48 18 12.73569	116 33 18.87387	631.404
PID_DH8974	48 18 01.45846	116 33 36.53568	633.046
AD9552	46 18 21.26105	119 18 36.67979	100.358
CRATES	45 39 7.47061	121 12 40.79288	45.918
86-19-305	46 11 52.54556	122 54 46.81341	-6.624
DEAControl	46 10 30.21870	123 9 54.56597	-13.656

2.2.2 RTK Survey

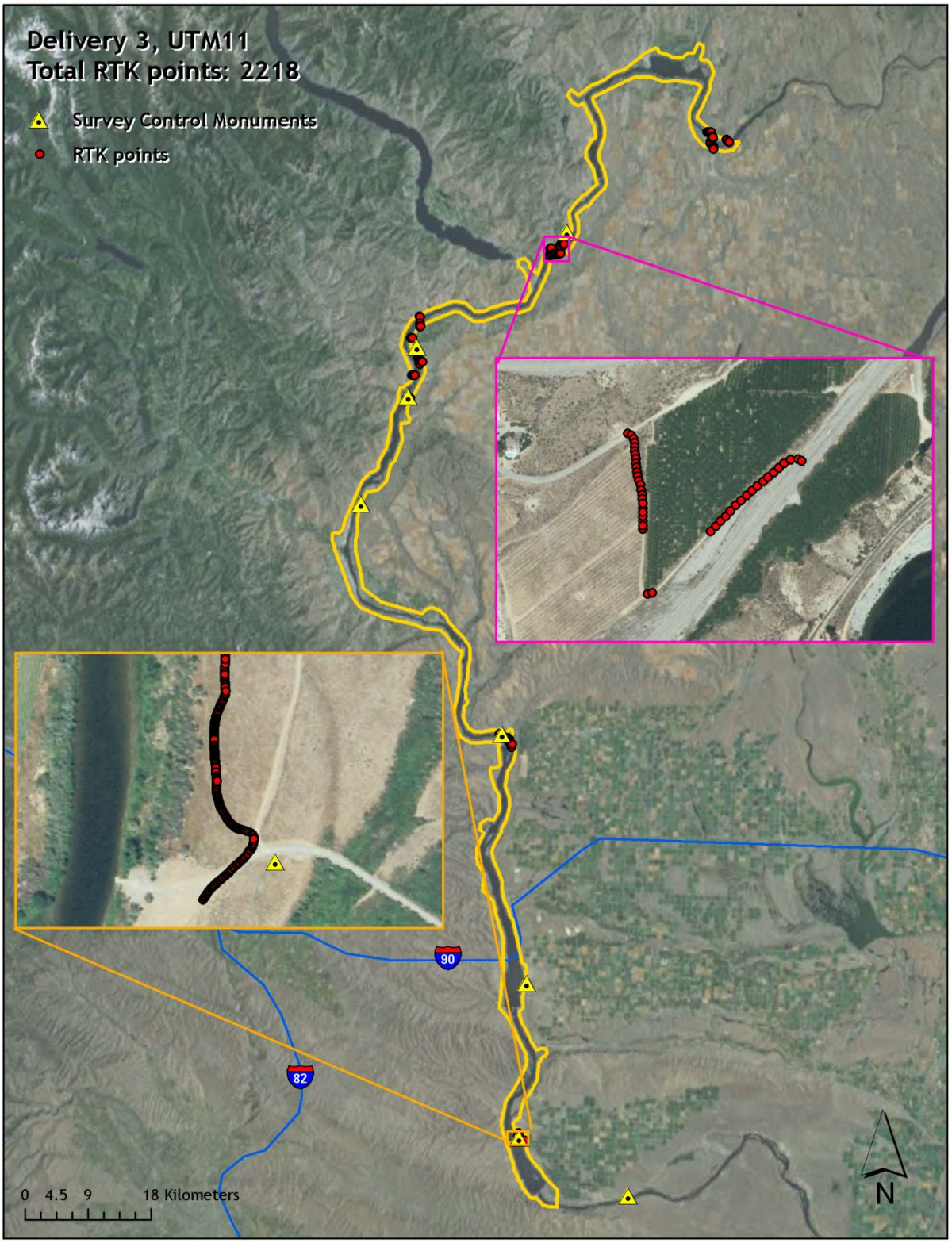
To enable assessment of LiDAR data accuracy, ground check points were collected using GPS based real-time kinematic (RTK) surveying. Instrumentation included multiple Trimble DGPS units (R8). RTK surveying allows for precise location measurements with an error (σ) of ≤ 1.5 cm (0.6 in).

For the RTK survey, the ground crew used a roving unit to receive radio-relayed corrected positional coordinates for all ground truth points from a GPS base station set up over certified survey control monuments. **Figure 2**, below, portrays the distribution of RTK point and basestation locations used for the current delivery of Columbia River survey areas. RTK points were collected on hard surfaces that were easily distinguishable within the LiDAR dataset. Paved surfaces, including roads, paths, and parking lots, were the primary surface target. After all paved surfaces had been exhausted, hard packed gravel roads became the secondary target for RTK, followed by hard packed dirt roads. Hard surfaces are targeted in areas that are clearly visible (and likely to remain visible) from the sky during data acquisition.

In order to facilitate comparisons with LiDAR data, RTK measurements were not taken on highly reflective surfaces such as center line stripes or lane markings on roads. RTK points were taken no closer than one meter to any nearby terrain breaks such as road edges or drop offs to ensure an accurate comparison between RTK and LiDAR ground data. In addition, attempts were made to collect RTK points on locations that could be readily identified and occupied during subsequent field visits. RTK measurements were collected approximately 1-2 meters from one another to support measurement independence.

An RTK point acquisition period is five seconds long and includes three individual one-second measurements averaged together. The five second observation period ensures that an accurate RTK point was taken. RTK points were not taken during periods when PDOP was greater than three, when less than six satellites were visible, or when horizontal and vertical RMS values were greater than 0.03 m. An RMS value of 0.03 m indicates that an RTK measurement is within 0.03 m of its actual position 68% of the time. An RTK check point was also taken at the beginning and end of each RTK session as close to the base station location as possible to provide an on-the-spot vertical accuracy check.

Figure 2. RTK point and control monument locations used in Delivery 3, UTM 11.



3. LiDAR Data Processing

3.1 Applications and Work Flow Overview

1. Resolved kinematic corrections for aircraft position data using kinematic aircraft GPS and static ground GPS data.

   Software: Waypoint GPS v.8.10, Trimble Geomatics Office v.1.62
2. Developed a smoothed best estimate of trajectory (SBET) file that blends post-processed aircraft position with attitude data Sensor head position and attitude were calculated throughout the survey. The SBET data were used extensively for laser point processing.

   Software: IPAS v.1.35
3. Calculated laser point position by associating SBET position to each laser point return time, scan angle, intensity, etc. Created raw laser point cloud data for the entire survey in *.las (ASPRS v. 1.2) format.

   Software: ALS Post Processing Software v.2.69
4. Imported raw laser points into manageable blocks (less than 500 MB) to perform manual relative accuracy calibration and filter for pits/birds. Ground points were then classified for individual flight lines (to be used for relative accuracy testing and calibration).

   Software: TerraScan v.10.009
5. Using ground classified points per each flight line, the relative accuracy was tested. Automated line-to-line calibrations were then performed for system attitude parameters (pitch, roll, heading), mirror flex (scale) and GPS/IMU drift. Calibrations were performed on ground classified points from paired flight lines. Every flight line was used for relative accuracy calibration.

   Software: TerraMatch v.10.006
6. Position and attitude data were imported. Resulting data were classified as ground and non-ground points. Statistical absolute accuracy was assessed via direct comparisons of ground classified points to ground RTK survey data. Data were then converted to orthometric elevations (NAVD88) by applying a Geoid03 correction. Ground models were created as a triangulated surface and exported as ArcInfo ASCII grids at a 1 –meter pixel resolution.

   Software: TerraScan v.10.009, ArcMap v. 9.3.1, TerraModeler v.10.004

3.2 Aircraft Kinematic GPS and IMU Data

LiDAR survey datasets were referenced to the 1 Hz static ground GPS data collected over pre-surveyed monuments with known coordinates. While surveying, the aircraft collected 2 Hz kinematic GPS data, and the onboard inertial measurement unit (IMU) collected 200 Hz aircraft attitude data. Waypoint GPS v.8.10 was used to process the kinematic corrections for the aircraft. The static and kinematic GPS data were then post-processed after the survey to obtain an accurate GPS solution and aircraft positions. IPAS v.1.35 was used to develop a trajectory file that includes corrected aircraft position and attitude information. The trajectory data for the entire flight survey session were incorporated into a final smoothed best estimated trajectory (SBET) file that contains accurate and continuous aircraft positions and attitudes.

3.3 Laser Point Processing

Laser point coordinates were computed using the IPAS and ALS Post Processor software suites based on independent data from the LiDAR system (pulse time, scan angle), and aircraft trajectory data (SBET). Laser point returns (first through fourth) were assigned an associated (x, y, z) coordinate along with unique intensity values (0-255). The data were output into large LAS v. 1.2 files; each point maintains the corresponding scan angle, return number (echo), intensity, and x, y, z (easting, northing, and elevation) information.

These initial laser point files were too large for subsequent processing. To facilitate laser point processing, bins (polygons) were created to divide the dataset into manageable sizes (< 500 MB). Flightlines and LiDAR data were then reviewed to ensure complete coverage of the survey area and positional accuracy of the laser points.

Laser point data were imported into processing bins in TerraScan, and manual calibration was performed to assess the system offsets for pitch, roll, heading and scale (mirror flex). Using a geometric relationship developed by Watershed Sciences, each of these offsets was resolved and corrected if necessary.

LiDAR points were then filtered for noise, pits (artificial low points) and birds (true birds as well as erroneously high points) by screening for absolute elevation limits, isolated points and height above ground. Each bin was then manually inspected for remaining pits and birds and spurious points were removed. In a bin containing approximately 7.5-9.0 million points, an average of 50-100 points are typically found to be artificially low or high. Common sources of non-terrestrial returns are clouds, birds, vapor, haze, decks, brush piles, etc.

Internal calibration was refined using TerraMatch. Points from overlapping lines were tested for internal consistency and final adjustments were made for system misalignments (i.e., pitch, roll, heading offsets and scale). Automated sensor attitude and scale corrections yielded 3-5 cm improvements in the relative accuracy. Once system misalignments were corrected, vertical GPS drift was then resolved and removed per flight line, yielding a slight improvement (<1 cm) in relative accuracy.

The TerraScan software suite is designed specifically for classifying near-ground points (Soininen, 2004). The processing sequence began by 'removing' all points that were not 'near' the earth based on geometric constraints used to evaluate multi-return points. The

resulting bare earth (ground) model was visually inspected and additional ground point modeling was performed in site-specific areas to improve ground detail. This manual editing of ground often occurs in areas with known ground modeling deficiencies, such as: bedrock outcrops, cliffs, deeply incised stream banks, and dense vegetation. In some cases, automated ground point classification erroneously included known vegetation (i.e., understory, low/dense shrubs, etc.). These points were manually reclassified as non-grounds. Ground surface rasters were developed from triangulated irregular networks (TINs) of ground points.

4. LiDAR Accuracy Assessment

Our LiDAR quality assurance process uses the data from the real-time kinematic (RTK) ground survey conducted in the survey area. For both the UTM 10 and UTM 11 areas delivered to date, a total of **11,007 RTK** GPS measurements were collected on hard surfaces distributed among multiple flight swaths. To assess absolute accuracy, we compared the location coordinates of these known RTK ground survey points to those calculated for the closest laser points.

4.1 Laser Noise and Relative Accuracy

Laser point absolute accuracy is largely a function of laser noise and relative accuracy. To minimize these contributions to absolute error, we first performed a number of noise filtering and calibration procedures prior to evaluating absolute accuracy.

Laser Noise

For any given target, laser noise is the breadth of the data cloud per laser return (i.e., last, first, etc.). Lower intensity surfaces (roads, rooftops, still/calm water) experience higher laser noise. The laser noise range for this survey was approximately 0.02 meters.

Relative Accuracy

Relative accuracy refers to the internal consistency of the data set - the ability to place a laser point in the same location over multiple flight lines, GPS conditions, and aircraft attitudes. Affected by system attitude offsets, scale, and GPS/IMU drift, internal consistency is measured as the divergence between points from different flight lines within an overlapping area. Divergence is most apparent when flight lines are opposing. When the LiDAR system is well calibrated, the line-to-line divergence is low (<10 cm). See Appendix A for further information on sources of error and operational measures that can be taken to improve relative accuracy.

Relative Accuracy Calibration Methodology

1. Manual System Calibration: Calibration procedures for each mission require solving geometric relationships that relate measured swath-to-swath deviations to misalignments of system attitude parameters. Corrected scale, pitch, roll and heading offsets were calculated and applied to resolve misalignments. The raw divergence between lines was computed after the manual calibration was completed and reported for each survey area.
2. Automated Attitude Calibration: All data were tested and calibrated using TerraMatch automated sampling routines. Ground points were classified for each individual flight line and used for line-to-line testing. System misalignment offsets (pitch, roll and

heading) and scale were solved for each individual mission and applied to respective mission datasets. The data from each mission were then blended when imported together to form the entire area of interest.

3. Automated Z Calibration: Ground points per line were used to calculate the vertical divergence between lines caused by vertical GPS drift. Automated Z calibration was the final step employed for relative accuracy calibration.

4.2 Absolute Accuracy

The vertical accuracy of the LiDAR data is described as the mean and standard deviation (sigma ~ σ) of divergence of LiDAR point coordinates from RTK ground survey point coordinates. To provide a sense of the model predictive power of the dataset, the root mean square error (RMSE) for vertical accuracy is also provided. These statistics assume the error distributions for x, y, and z are normally distributed, thus we also consider the skew and kurtosis of distributions when evaluating error statistics.

Statements of statistical accuracy apply to fixed terrestrial surfaces only and may not be applied to areas of dense vegetation or steep terrain. To calibrate laser accuracy for the Delivery 3 LiDAR dataset, 2218 RTK points were collected on fixed, hard-packed road surfaces within the survey area.

5. Study Area Results

Summary statistics for point resolution and accuracy (relative and absolute) of the LiDAR data collected in the Columbia River survey areas are presented below in terms of central tendency, variation around the mean, and the spatial distribution of the data (for point resolution by quadrangle).

5.1 Data Summary

Table 3. Resolution and Accuracy - Specifications and Achieved Values

	Targeted	Achieved
Resolution:		
UTM 11	≥ 8 points/m^2	6.76 points/m^2
***Vertical Accuracy (1 σ):**		
UTM 11	<13 cm	3.5 cm

* Based on 6024 hard-surface control points within UTM 11

5.2 Data Density/Resolution

The average first-return density of the UTM 11 delivered dataset is 6.76 points per square meter (**Table 3**). The initial dataset, acquired to be 8 points per square meter, was filtered as described previously to remove spurious or inaccurate points. Additionally, some types of surfaces (i.e., dense vegetation, breaks in terrain, steep slopes, water) may return fewer pulses (delivered density) than the laser originally emitted (native density). Due to the fact that this survey focused on a narrow corridor buffering the Columbia River, the reported first return density is artificially low.

Ground classifications were derived from automated ground surface modeling and manual, supervised classifications where it was determined that the automated model had failed. Ground return densities will be lower in areas of dense vegetation, water, or buildings.
The maps in **Figures 5 - 12** identify the average native and ground point densities for each USGS 0.75 minute quad. Tiles with greater than 20 million points were divided in half to keep LAS file sizes manageable.

Cumulative LiDAR data resolution for UTM 11 of the Columbia River survey:

- Average Point (First Return) Density = 6.76 points/m^2
- Average Ground Point Density = 1.95 points/m^2

Figure 3. Density distribution for first return laser points in UTM 11.

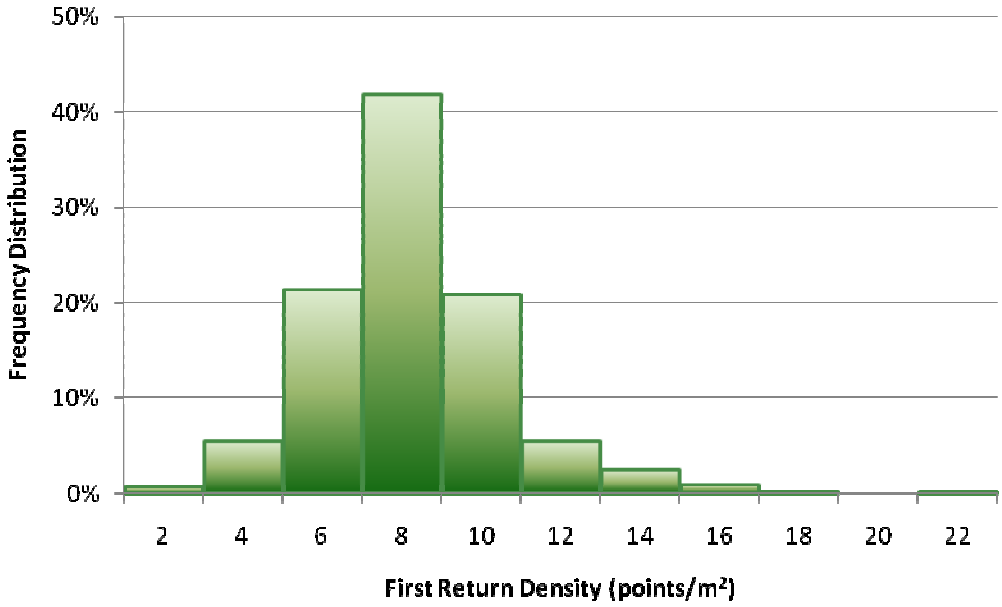


Figure 4. Density distribution for ground-classified laser points in, UTM 11.

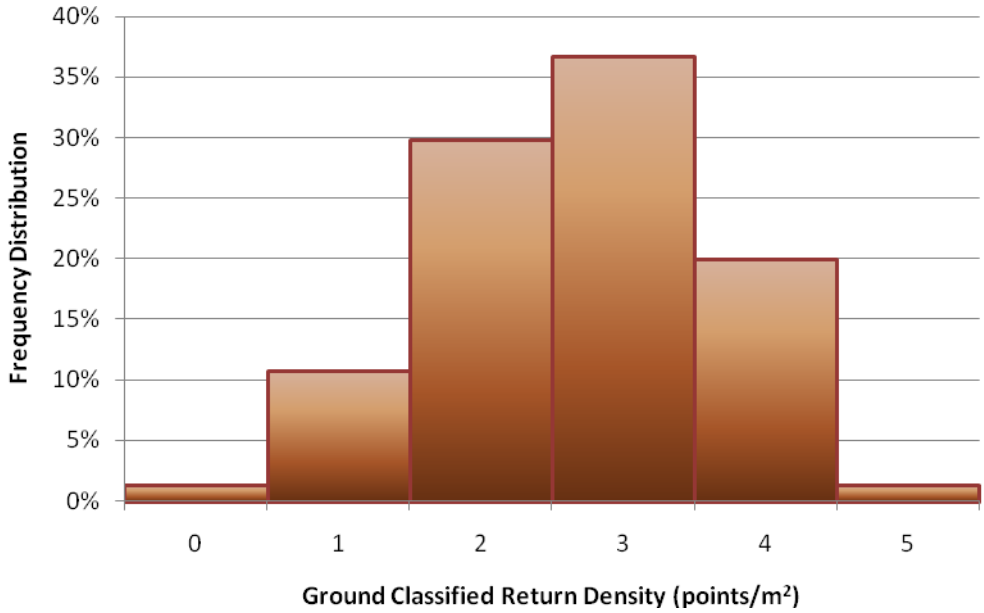


Figure 5. Delivery 1, UTM 10 density distribution map for first return points by USGS 0.75 minute quads.

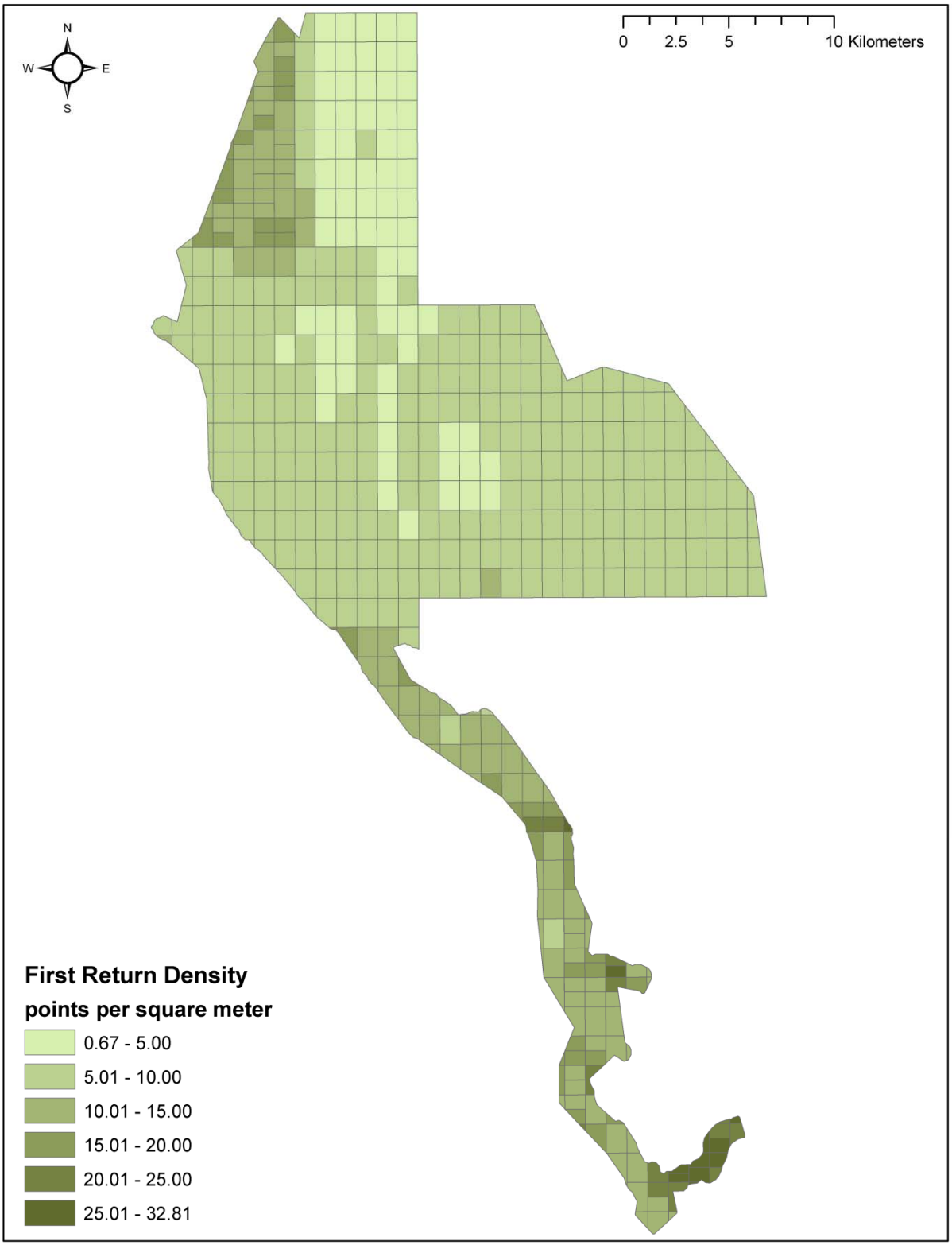


Figure 6. Delivery 1, UTM 10 density distribution map for ground return points by USGS 0.75 minute quads.

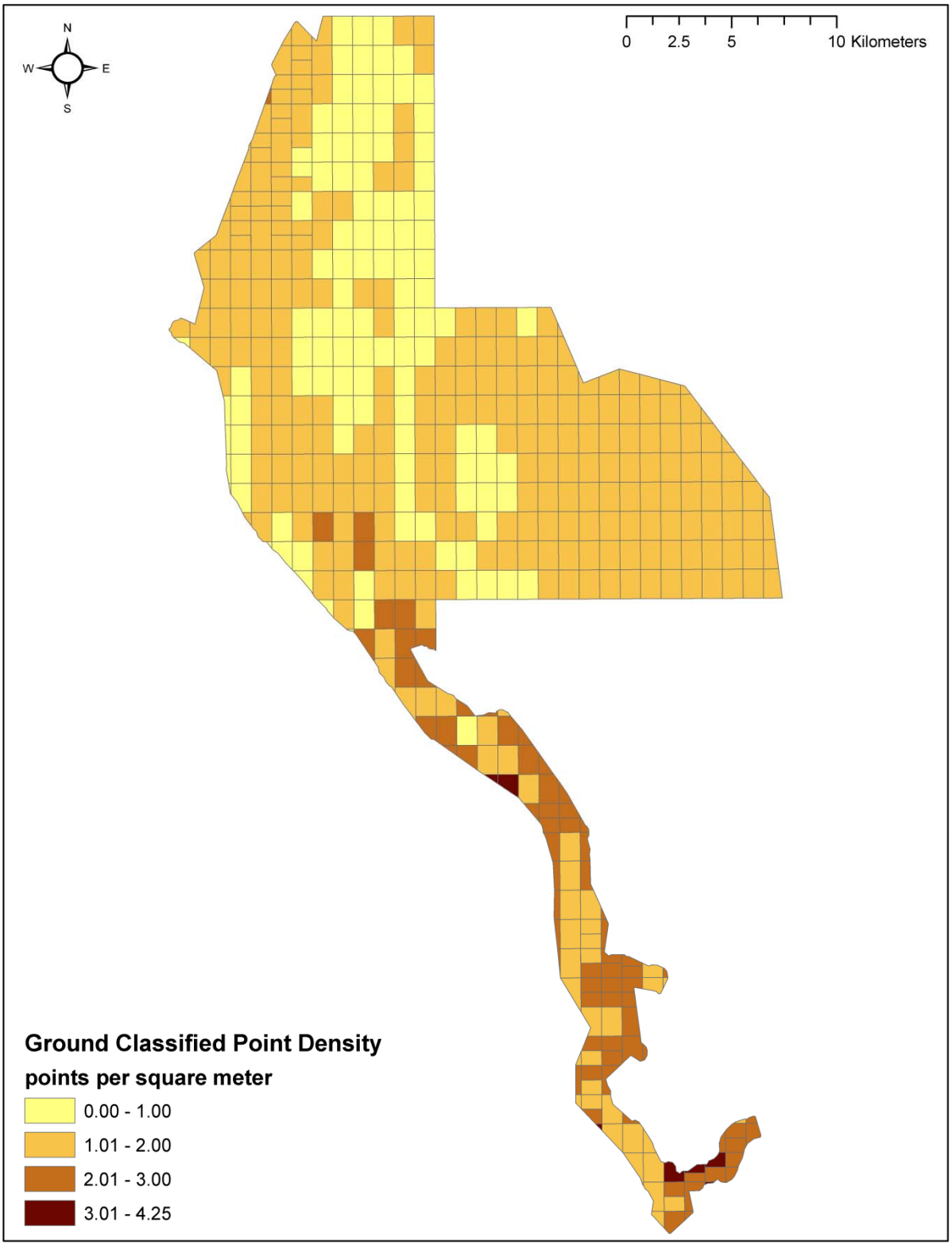


Figure 7. Delivery 1, UTM 11 density distribution map for first return points by USGS 0.75 minute quads.

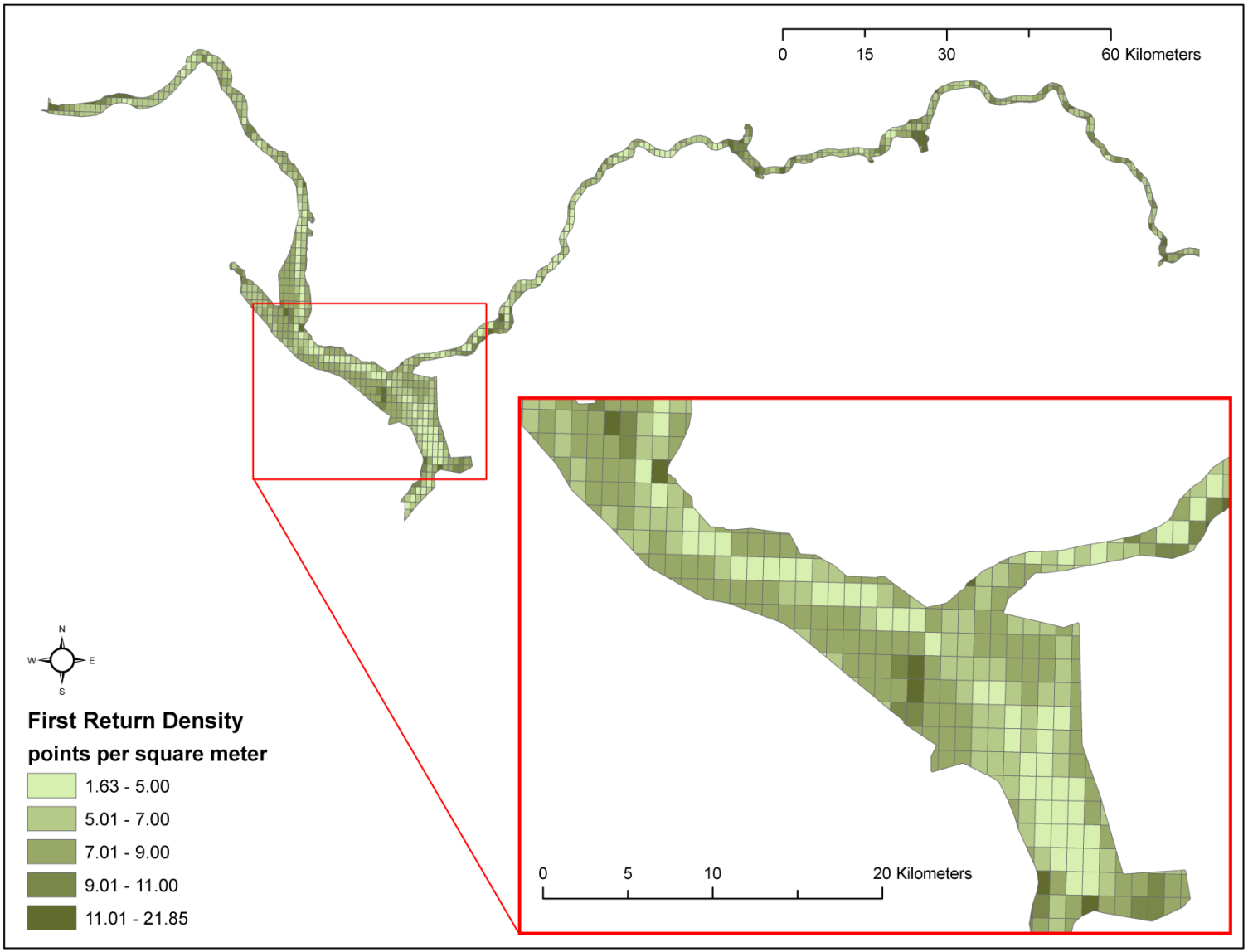


Figure 8. Delivery 1, UTM 11 density distribution map for ground return points by USGS 0.75 minute quads.

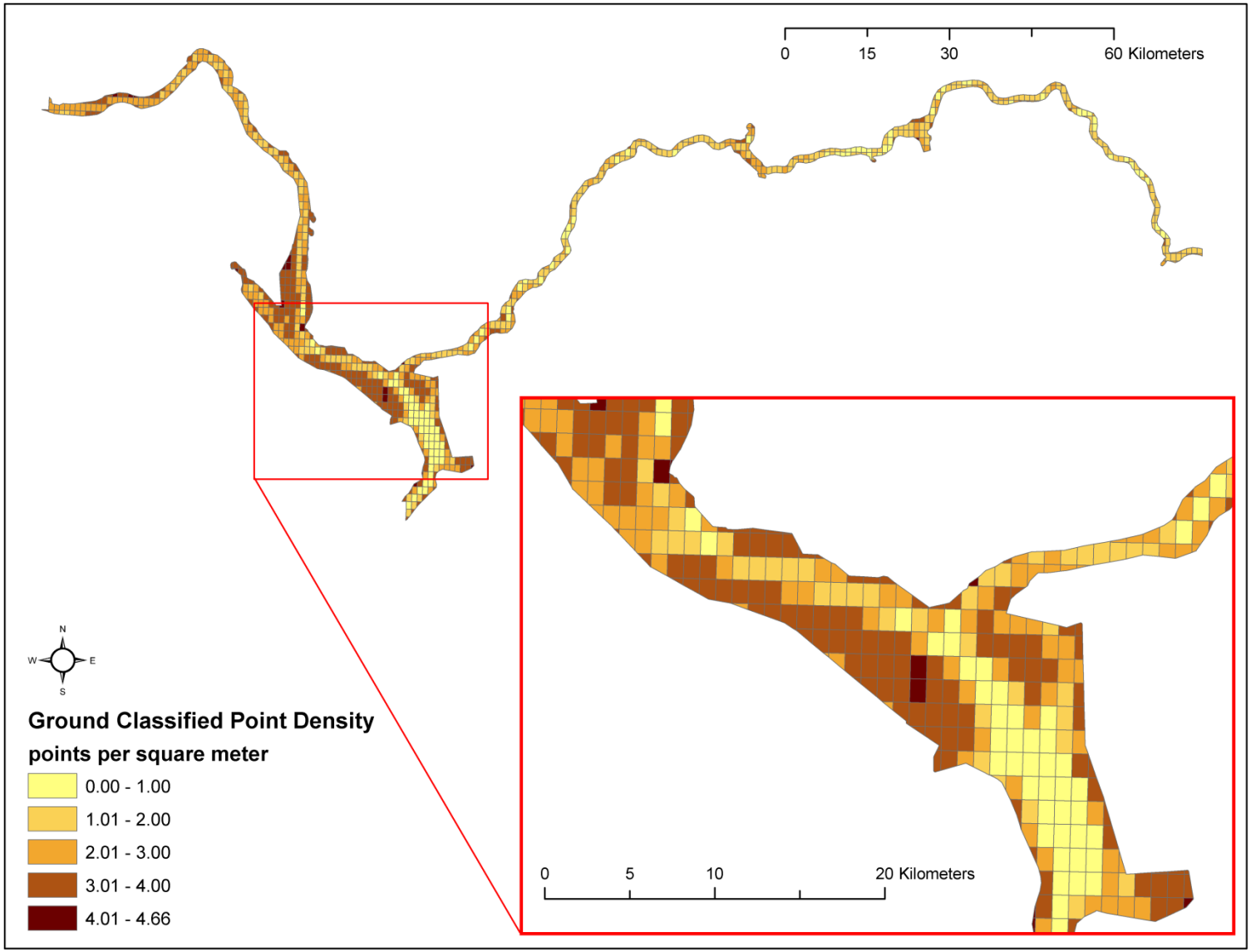


Figure 9. Delivery 2, UTM 10 density distribution map for first return points by USGS 0.75 minute quads.

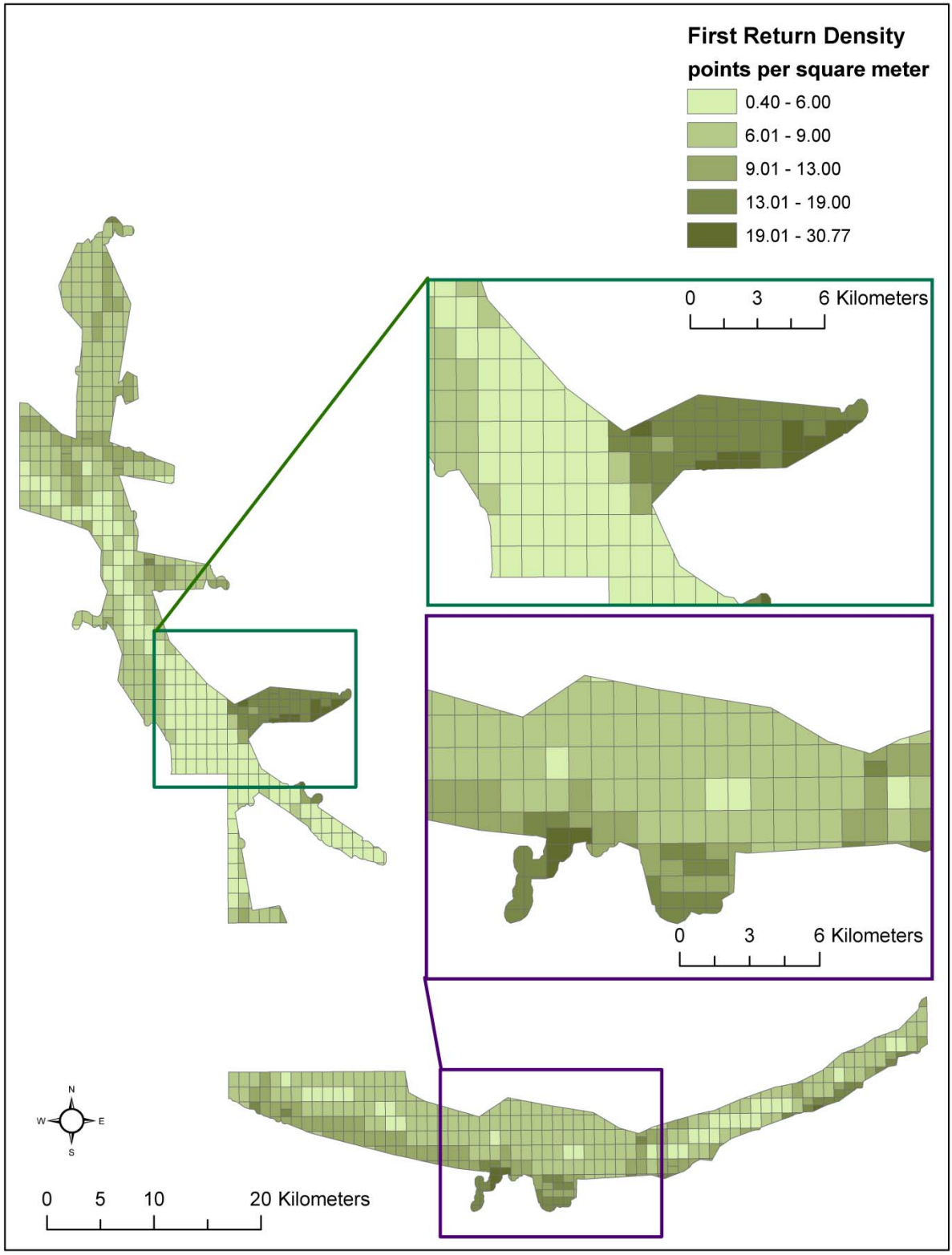


Figure 10. Delivery 2, UTM 10 density distribution map for ground return points by USGS 0.75 minute quads.

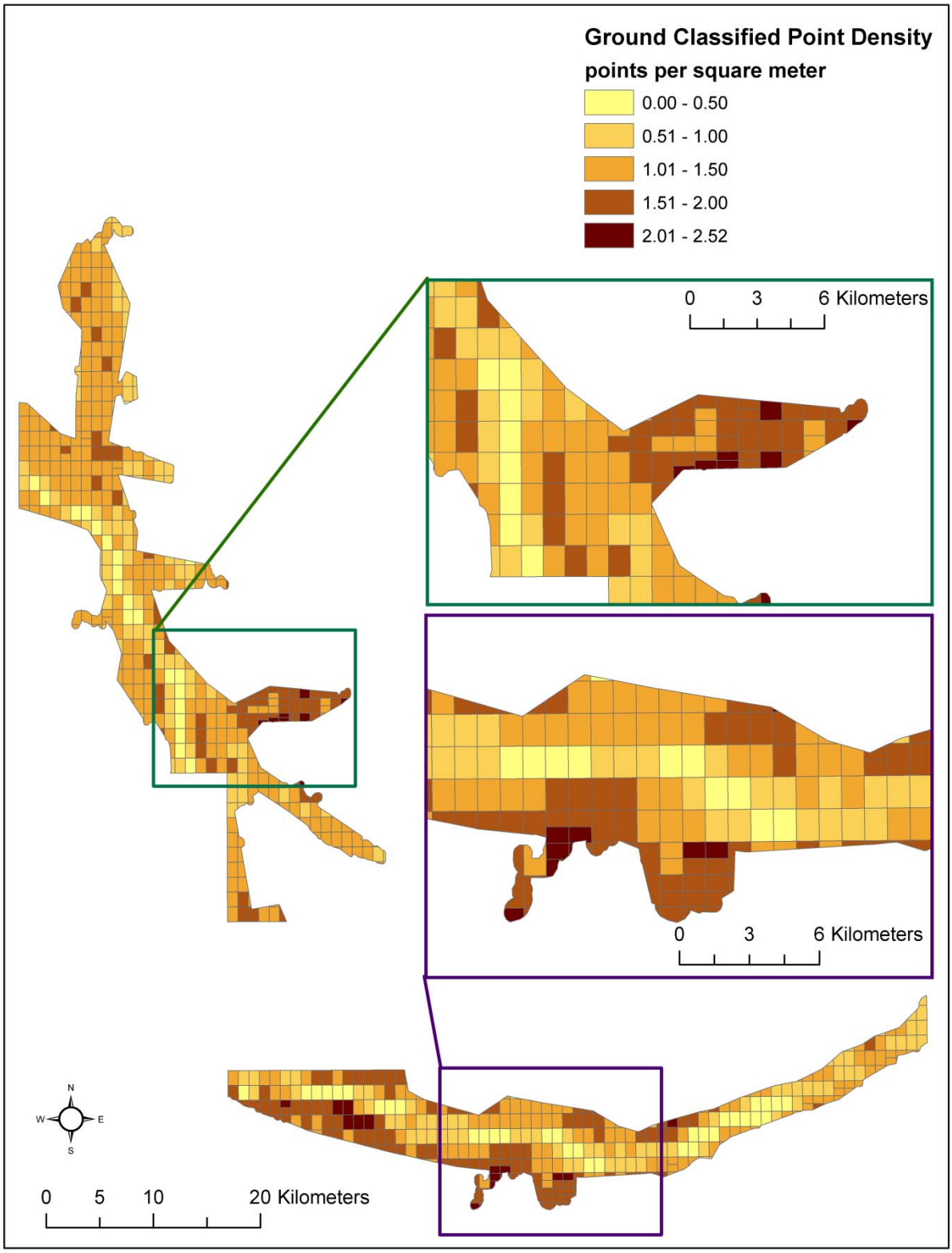


Figure 11. Delivery 3, UTM 11 density distribution map for first return points by USGS 0.75 minute quads

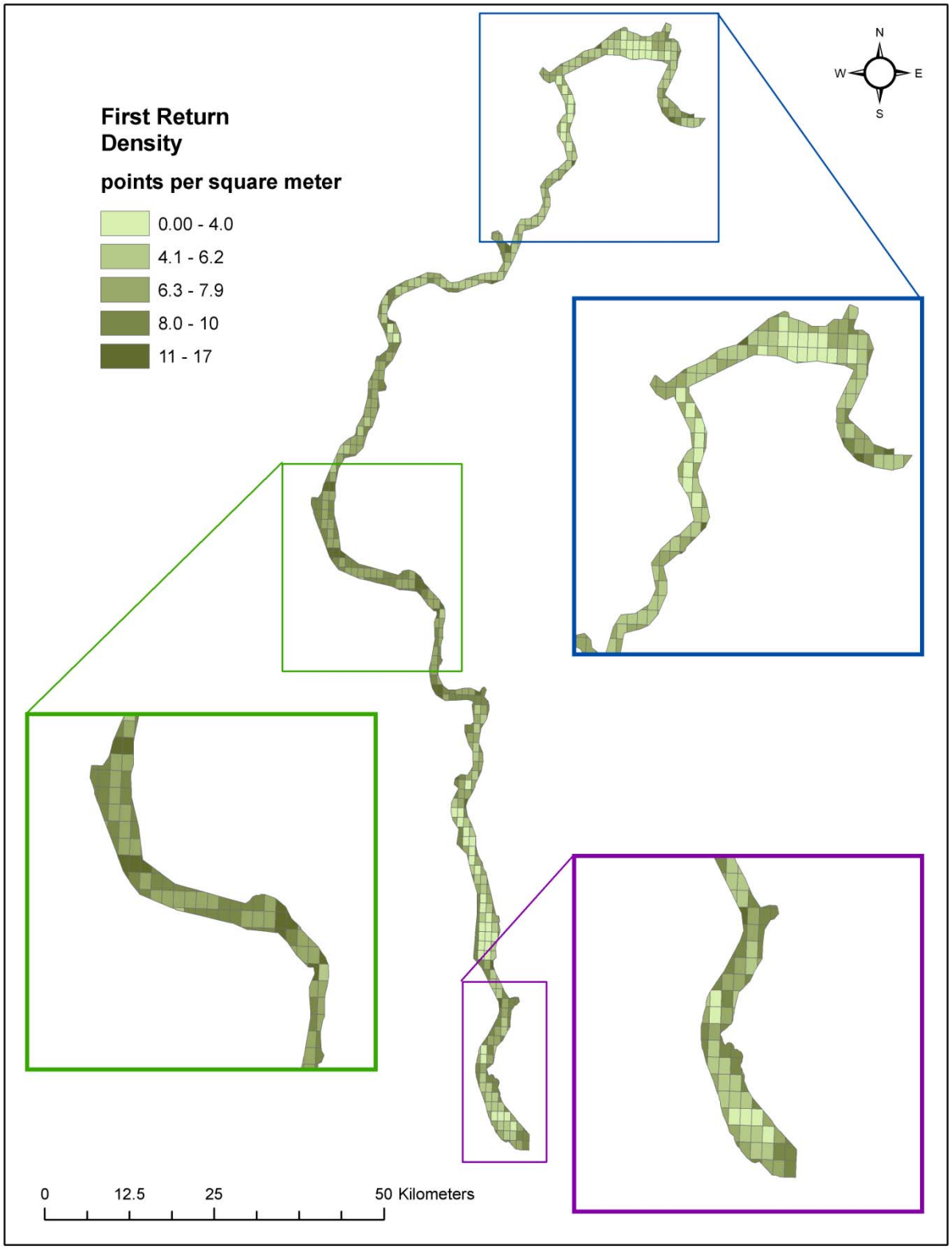
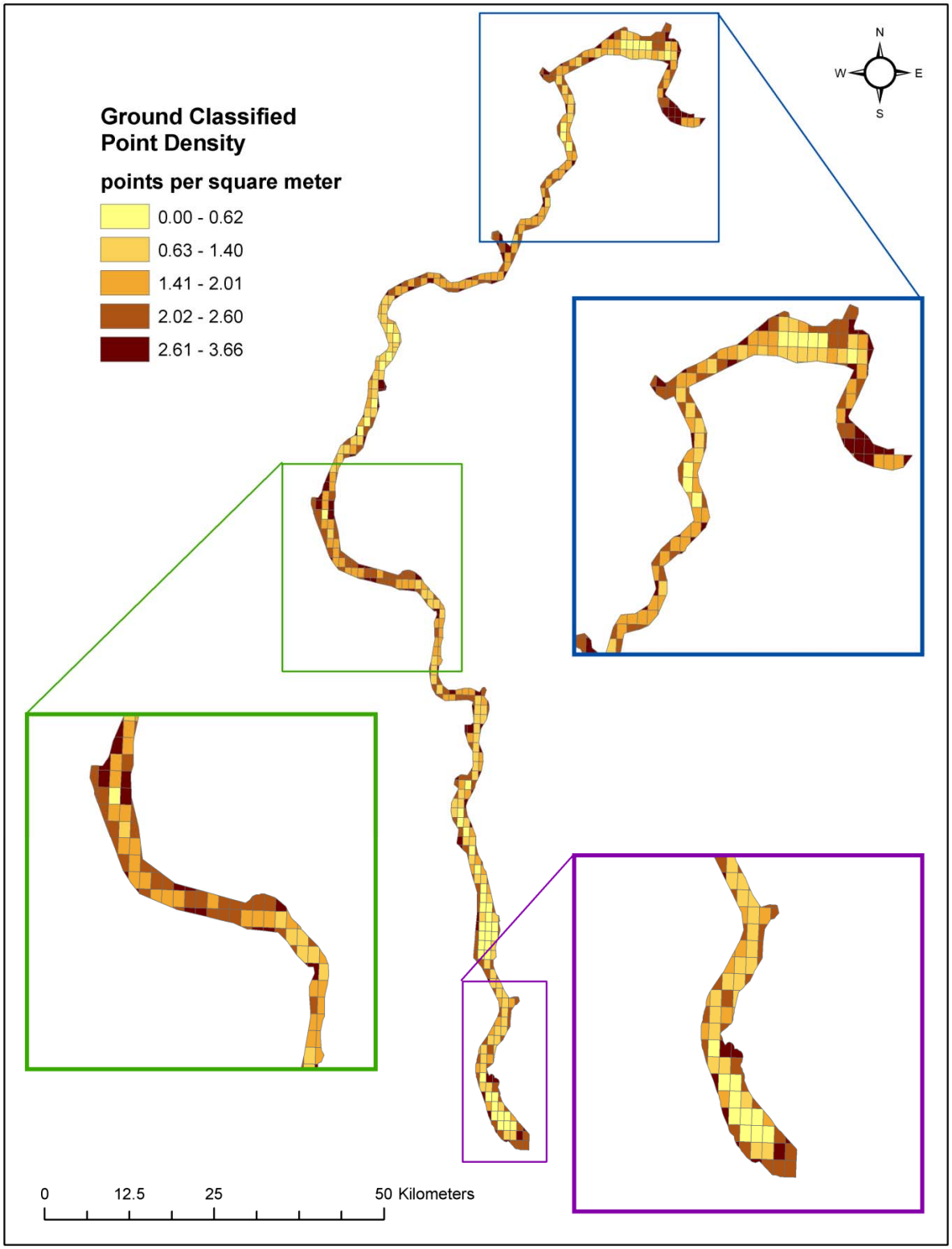


Figure 12. Delivery 3, UTM 11 density distribution map for ground return points by USGS 0.75 minute quads.



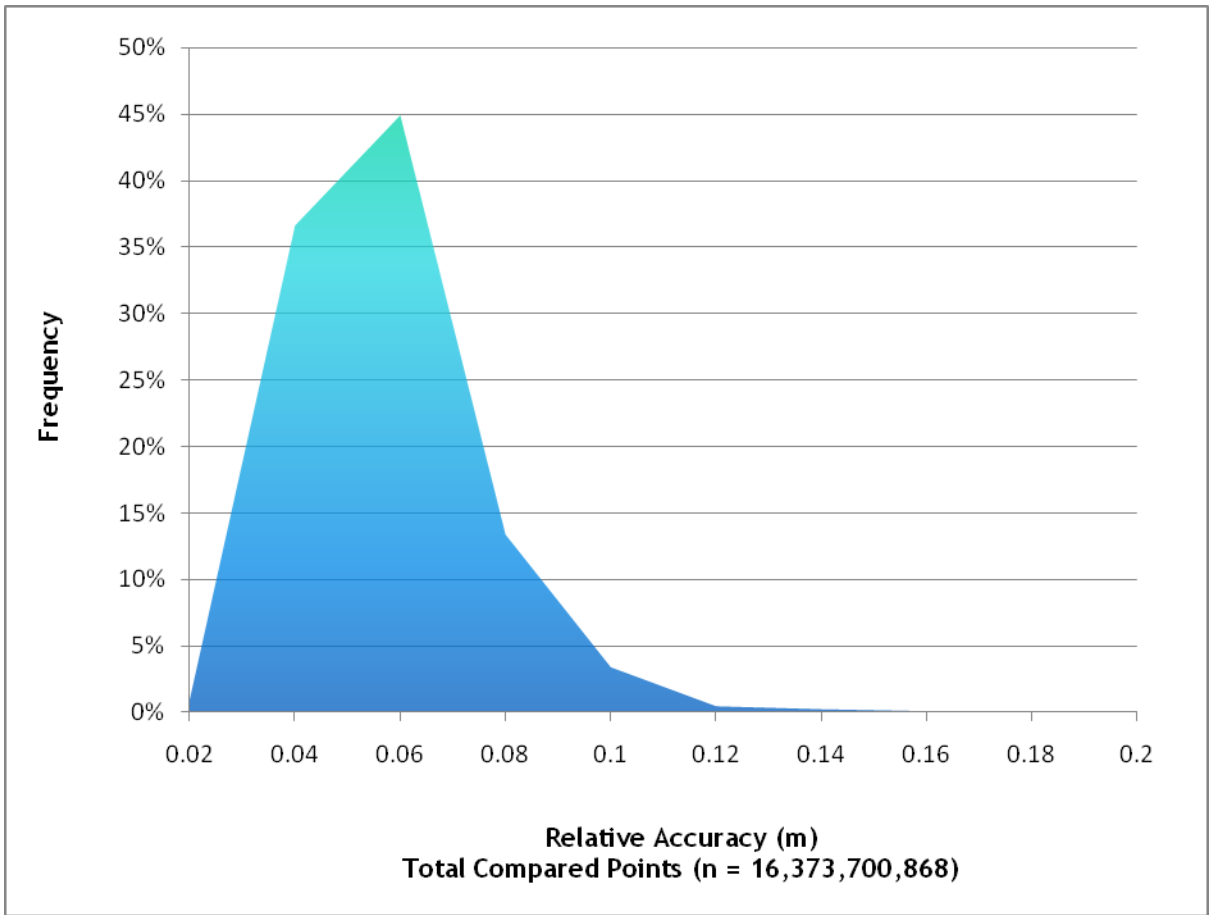
5.3 Relative Accuracy Calibration Results

Relative accuracies for the Columbia River survey area measure the full survey calibration including areas outside the delivered boundary.

Relative accuracy statistics for UTM 11 delivered to date

- Project Average = 0.044m
- Median Relative Accuracy = 0.044m
- 1σ Relative Accuracy = 0.050m
- 2σ Relative Accuracy = 0.079m

Figure 13. Distribution of relative accuracies per flight line, non slope-adjusted for UTM 11



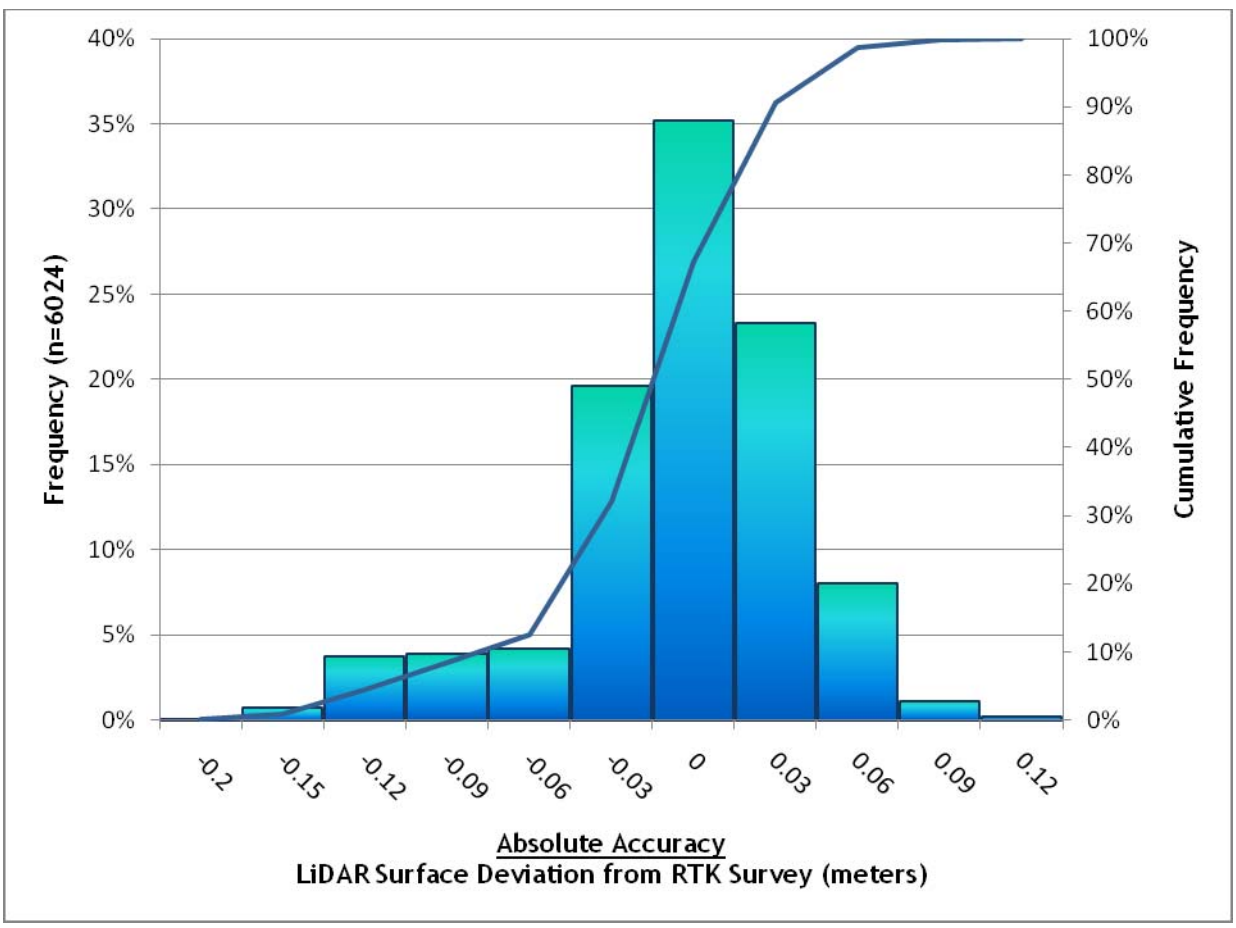
5.4 Absolute Accuracy

Absolute accuracies for the Columbia River survey areas:

Table 4. Absolute Accuracy for UTM 11 – Deviation between laser points and RTK hard surface survey points

RTK Survey Sample Size (n): 6024	
Root Mean Square Error (RMSE) = (0.047m)	Minimum Δz = -0.208m
Standard Deviations 1 sigma (σ): (0.035m) 2 sigma (σ): (0.115m)	Maximum Δz = 0.111m Average Δz = -0.019m

Figure 14. Absolute Accuracy - Histogram Statistics, based on 6024 RTK points in UTM 11



6. Breakline Enforced Terrain Model

David C. Smith and Associates (DSA) created breaklines for the Columbia River study area using LiDAR-grammetry techniques. **Table 5** describes the type and definition of each breakline collected. The breaklines were used to supplement the LiDAR data in creation of a final ground model. Water boundaries were enforced using hard breaklines and water surfaces were flattened based on the elevation from the breaklines. The breakline boundaries were also used to class any points with ground or model key point classification within the water delineated areas.

Table 5. Breaklines collected for the Columbia River study area, see Appendix B for feature definitions.

Feature	Implementation
Breakline	Hard Breakline
Breakline Obscured	Hard Breakline
Water Main	Hard Breakline
Water Island	Hard Breakline
Water Other	Hard Breakline
Buildings	Provided as Feature

7. Projection/Datum and Units

	Projection:	UTM Zone 10 and 11, NAD 83
Datum	**Vertical:**	NAVD88 Geoid09
	Horizontal:	NAD83
	Units:	meters

8. Deliverables

Point Data:	• All Returns (LAS 1.2 format)
Vector Data:	• Tile Index of LiDAR points (USGS 0.75 minute quads, shapefile) • Tile Index of DEM rasters (USGS 7.5 minute quads, shapefile) • 1-hz SBET files (shapefile) • Breaklines (dxf format) *provided by DSA* • Watermask (dxf.format) *provided by DSA*

Raster Data:	• Elevation models (1 m resolution)
	  • Breakline Enforced Bare Earth Model (ESRI GRID format)
	  • Highest Hit Model (ESRI GRID format)
	• Intensity images (GeoTIFF format, 1 m resolution)

Data Report:	Full report containing introduction, methodology, and accuracy

9. Selected Images

Figure 15. 3D view looking East along the Methow River. Top image is 2006 NAIP draped over highest hit model, bottom image is a bare earth model colored by elevation.

Figure 16. 3D view looking west along Brushy Creek, the bare earth image is colored by elevation.

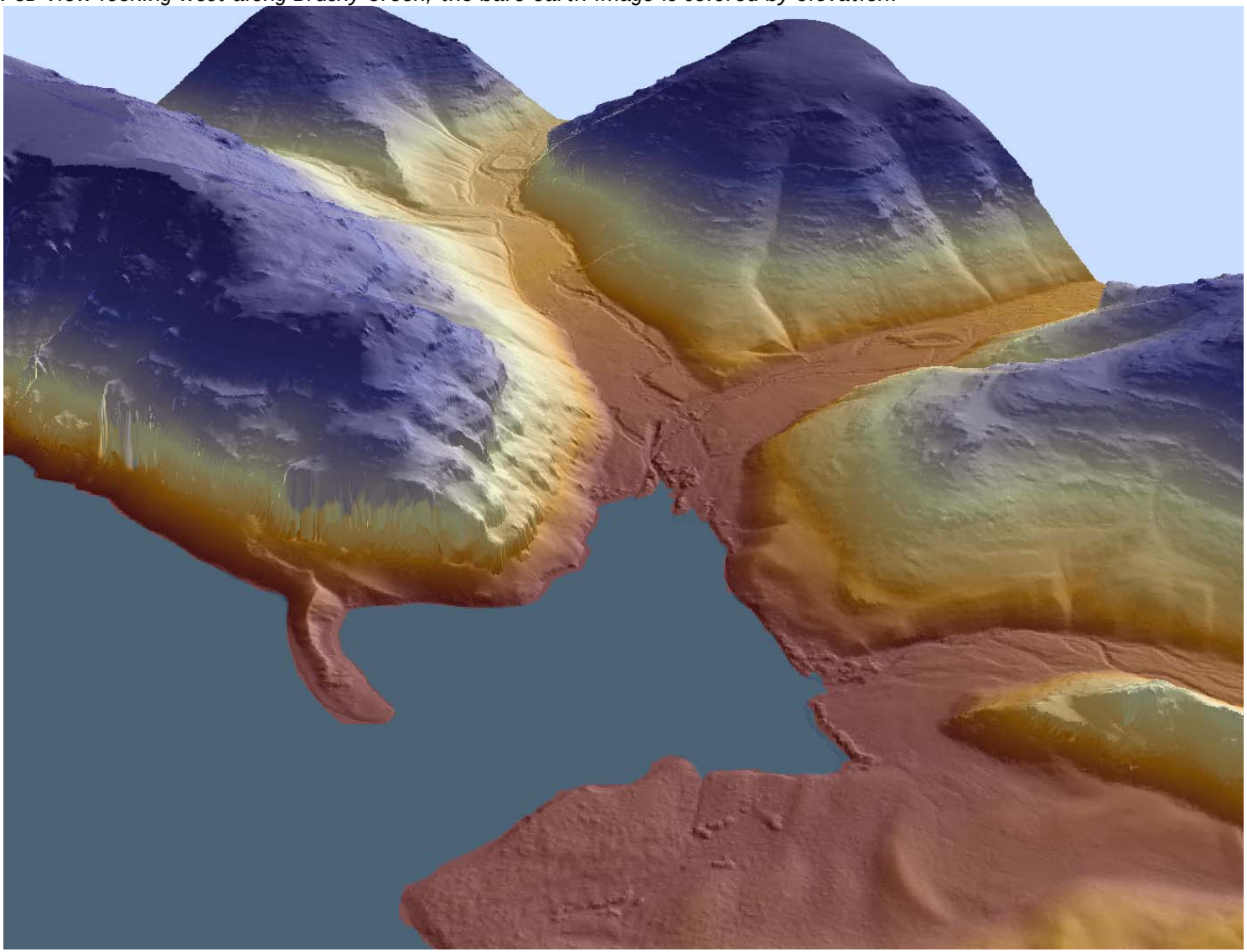


Figure 17. 3D view looking North up the Columbia River with views of Locke Island near Hanford Reach. Top image derived from ground-classified LiDAR points, bottom image derived from highest-hit LiDAR points colored by NAIP imagery.

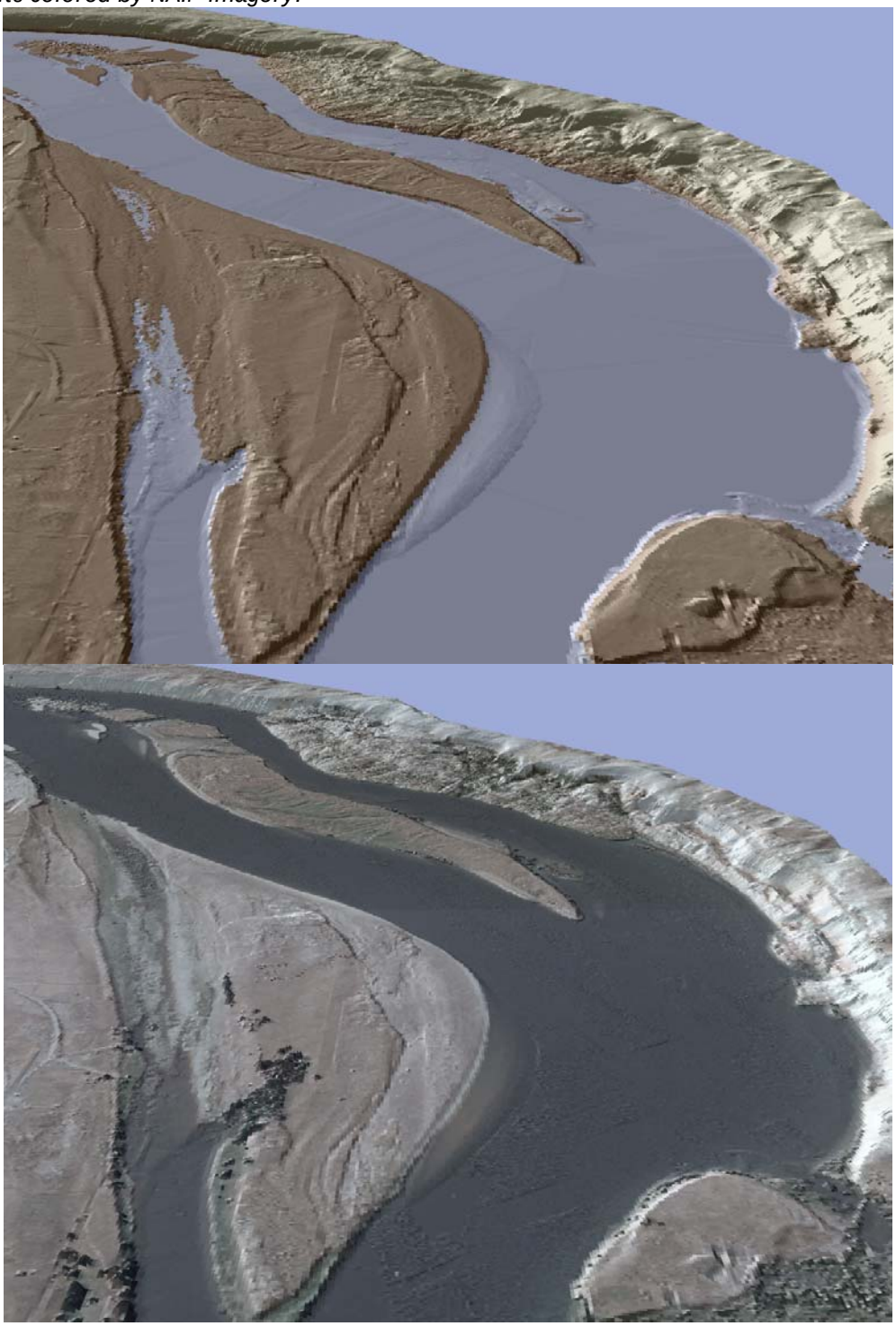


Figure 18. 3D view looking North west over Richland, WA with views of Bateman Island and Riverview and Chamna Nature Preserves . Top image derived from ground-classified LiDAR points, bottom image derived from highest-hit LiDAR points.

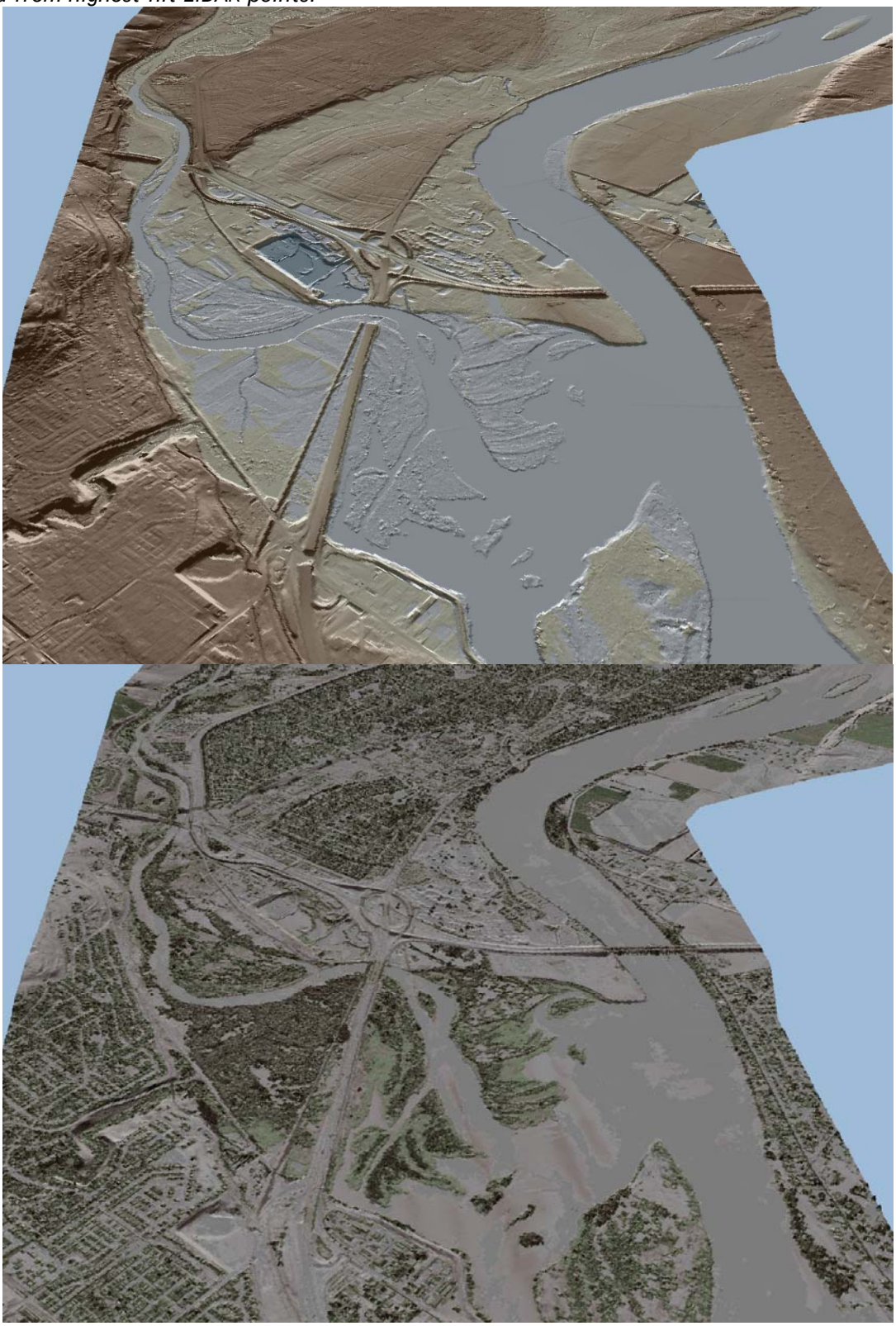


Figure 19. 3D point cloud looking north at I-5 crossing the Columbia River. MLK Blvd can be seen over I-5 and Portland Harbor is in the distance.

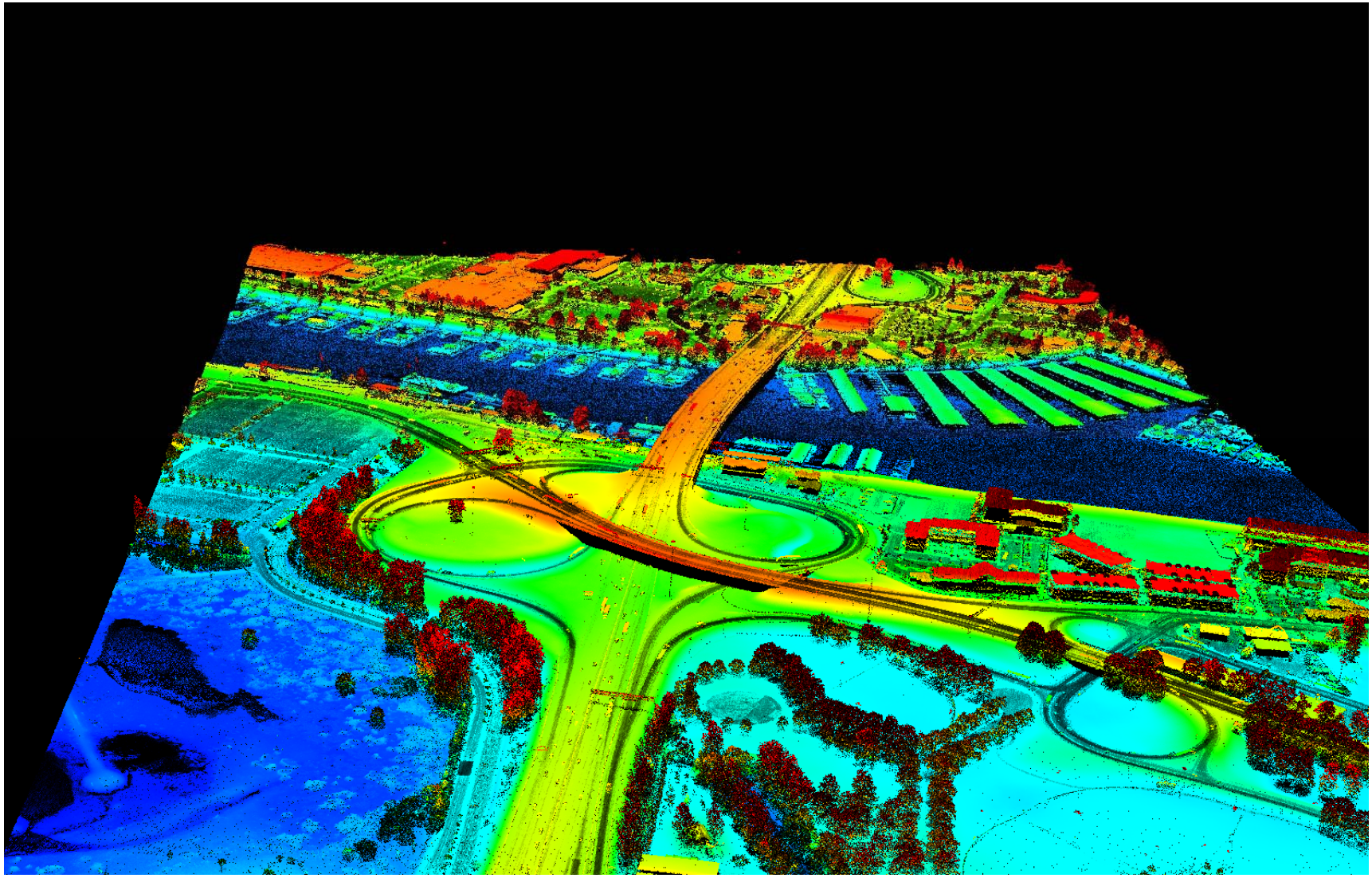


Figure 20. 3D point cloud looking southeast at middle section of Hayden island. A railroad bridge can be seen crossing the Columbia River with Portland Harbor in the far distant corner.

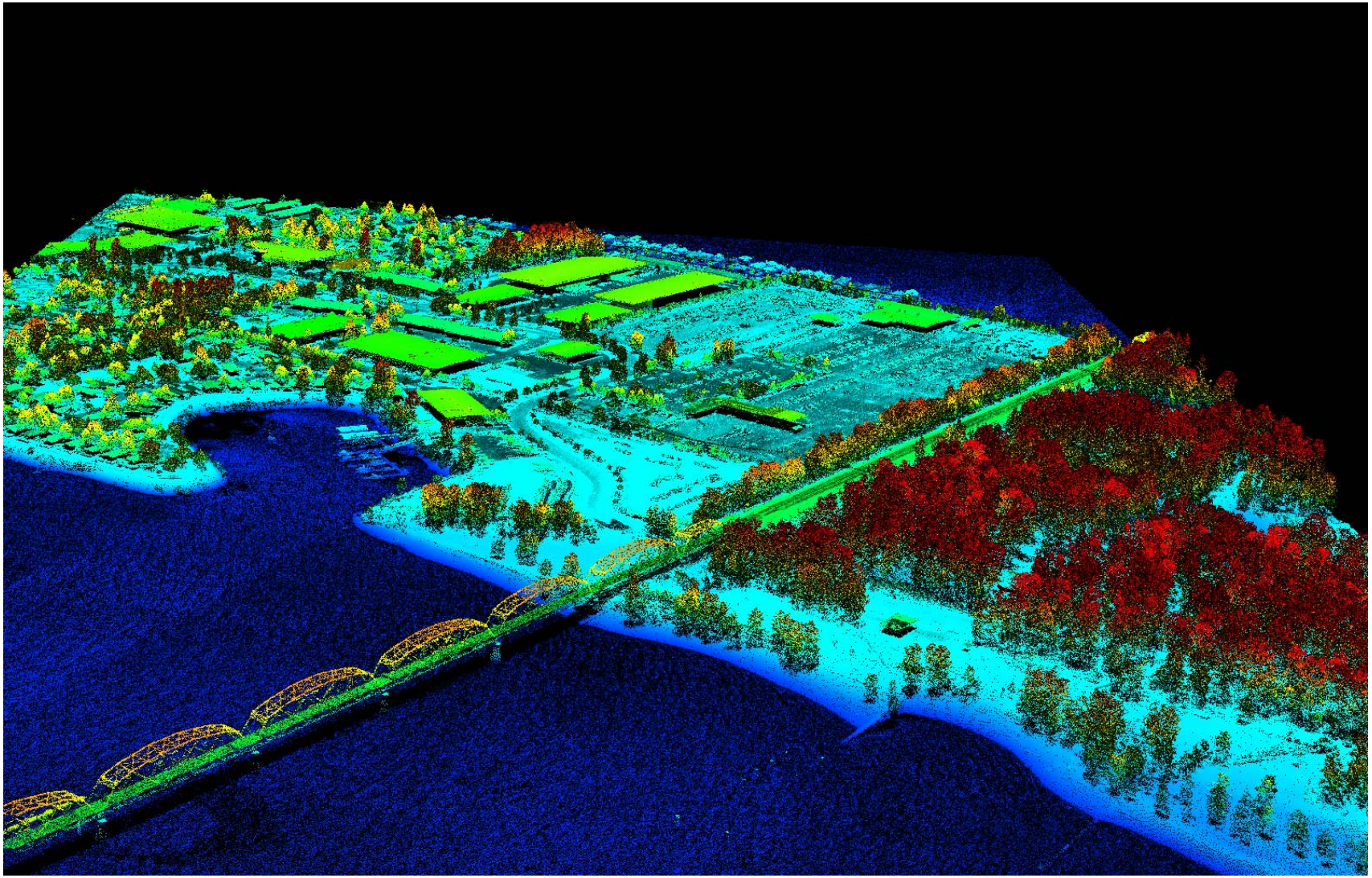
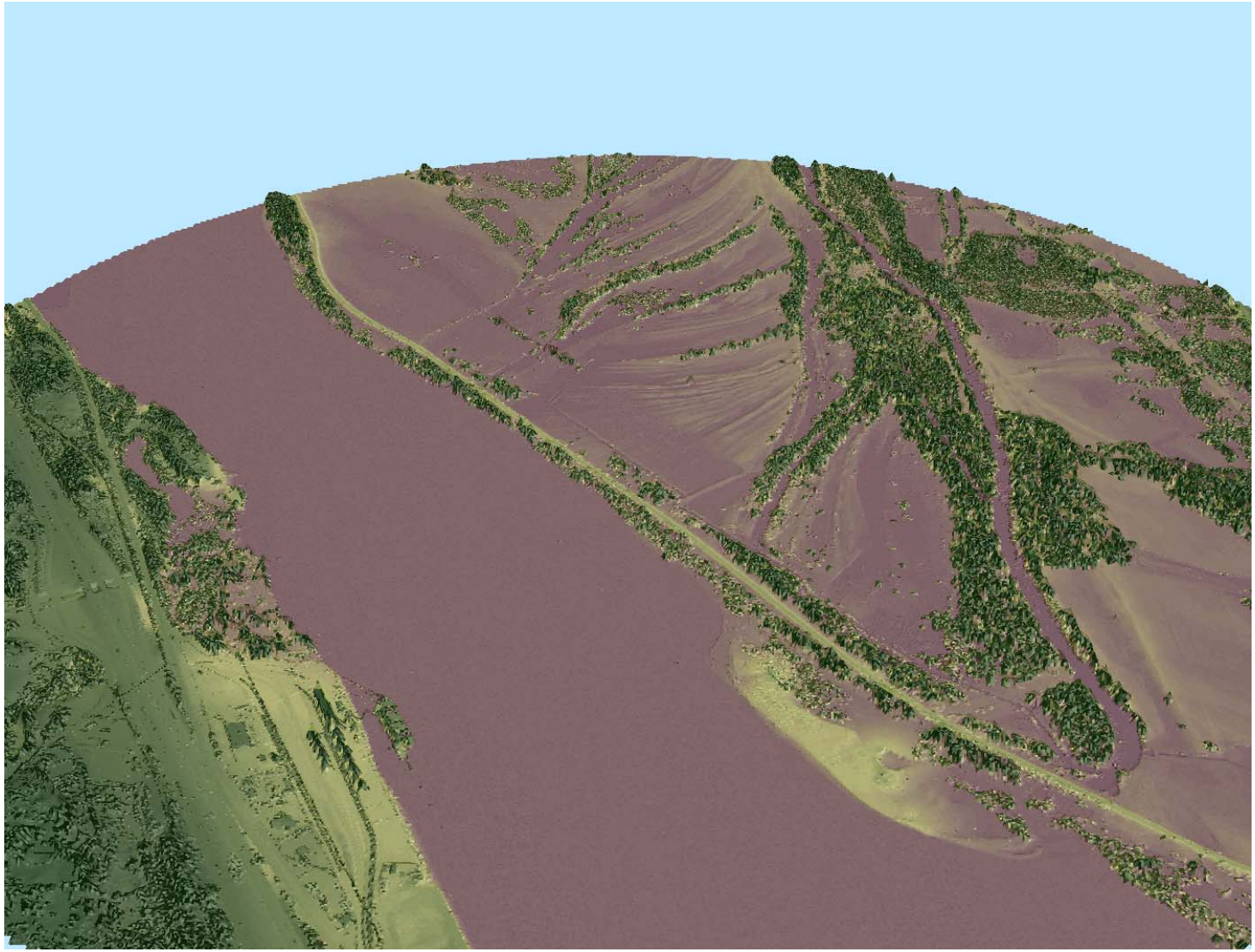


Figure 21. Highest hit model looking South along the Columbia River. Drainage patterns on the right hand side highlight Cottonwood Lake and Swan Lake. Daves Slough is on the far right hand side of image. Looking at Deer Island from Washington border.



10. Glossary

1-sigma (σ) Absolute Deviation: Value for which the data are within one standard deviation (approximately 68th percentile) of a normally distributed data set.

2-sigma (σ) Absolute Deviation: Value for which the data are within two standard deviations (approximately 95th percentile) of a normally distributed data set.

Root Mean Square Error (RMSE): A statistic used to approximate the difference between real-world points and the LiDAR points. It is calculated by squaring all the values, then taking the average of the squares and taking the square root of the average.

Pulse Rate (PR): The rate at which laser pulses are emitted from the sensor; typically measured as thousands of pulses per second (kHz).

Pulse Returns: For every laser pulse emitted, the Leica ALS 50 Phase II system can record *up to four* wave forms reflected back to the sensor. Portions of the wave form that return earliest are the highest element in multi-tiered surfaces such as vegetation. Portions of the wave form that return last are the lowest element in multi-tiered surfaces.

Accuracy: The statistical comparison between known (surveyed) points and laser points. Typically measured as the standard deviation (sigma, σ) and root mean square error (RMSE).

Intensity Values: The peak power ratio of the laser return to the emitted laser. It is a function of surface reflectivity.

Data Density: A common measure of LiDAR resolution, measured as points per square meter.

Spot Spacing: Also a measure of LiDAR resolution, measured as the average distance between laser points.

Nadir: A single point or locus of points on the surface of the earth directly below a sensor as it progresses along its flight line.

Scan Angle: The angle from nadir to the edge of the scan, measured in degrees. Laser point accuracy typically decreases as scan angles increase.

Overlap: The area shared between flight lines, typically measured in percents; 100% overlap is essential to ensure complete coverage and reduce laser shadows.

DTM / DEM: These often-interchanged terms refer to models made from laser points. The digital elevation model (DEM) refers to all surfaces, including bare ground and vegetation, while the digital terrain model (DTM) refers only to those points classified as ground.

Real-Time Kinematic (RTK) Survey: GPS surveying is conducted with a GPS base station deployed over a known monument with a radio connection to a GPS rover. Both the base station and rover receive differential GPS data and the baseline correction is solved between the two. This type of ground survey is accurate to 1.5 cm or less.

11. Citations

Soininen, A. 2004. TerraScan User's Guide. TerraSolid.

Appendix A

LiDAR accuracy error sources and solutions:

Type of Error	Source	Post Processing Solution
GPS (Static/Kinematic)	Long Base Lines	None
	Poor Satellite Constellation	None
	Poor Antenna Visibility	Reduce Visibility Mask
Relative Accuracy	Poor System Calibration	Recalibrate IMU and sensor offsets/settings
	Inaccurate System	None
Laser Noise	Poor Laser Timing	None
	Poor Laser Reception	None
	Poor Laser Power	None
	Irregular Laser Shape	None

Operational measures taken to improve relative accuracy:

1. Low Flight Altitude: Terrain following is employed to maintain a constant above ground level (AGL). Laser horizontal errors are a function of flight altitude above ground (i.e., ~ 1/3000th AGL flight altitude).
2. Focus Laser Power at narrow beam footprint: A laser return must be received by the system above a power threshold to accurately record a measurement. The strength of the laser return is a function of laser emission power, laser footprint, flight altitude and the reflectivity of the target. While surface reflectivity cannot be controlled, laser power can be increased and low flight altitudes can be maintained.
3. Reduced Scan Angle: Edge-of-scan data can become inaccurate. The scan angle was reduced to a maximum of ±15° from nadir, creating a narrow swath width and greatly reducing laser shadows from trees and buildings.
4. Quality GPS: Flights took place during optimal GPS conditions (e.g., 6 or more satellites and PDOP [Position Dilution of Precision] less than 3.0). Before each flight, the PDOP was determined for the survey day. During all flight times, a dual frequency DGPS base station recording at 1–second epochs was utilized and a maximum baseline length between the aircraft and the control points was less than 19 km (11.5 miles) at all times.
5. Ground Survey: Ground survey point accuracy (i.e. <1.5 cm RMSE) occurs during optimal PDOP ranges and targets a minimal baseline distance of 4 miles between GPS rover and base. Robust statistics are, in part, a function of sample size (n) and distribution. Ground survey RTK points are distributed to the extent possible throughout multiple flight lines and across the survey area.
6. 50% Side-Lap (100% Overlap): Overlapping areas are optimized for relative accuracy testing. Laser shadowing is minimized to help increase target acquisition from multiple scan angles. Ideally, with a 50% side-lap, the most nadir portion of one flight line coincides with the edge (least nadir) portion of overlapping flight lines. A minimum of 50% side-lap with terrain-followed acquisition prevents data gaps.
7. Opposing Flight Lines: All overlapping flight lines are opposing. Pitch, roll and heading errors are amplified by a factor of two relative to the adjacent flight line(s), making misalignments easier to detect and resolve.

Appendix B

Breakline definitions as determined by DSA:

FEATURE:

BREAKLINE - Added to the ground model where the LiDAR ground points were missing or not properly defining the surface. Usually occured on sharp breaks associated with cliffs. These breaks are derived from the 1st return data and fit to the ground data.

BREAKLINE_OBSCURE - Added in vegetated areas where the LiDAR ground model was not complete due to dense vegetation. These lines are interpreted from visible data and fit to visible ground data.

WATER_MAIN - Main rivers, not including side rivers and streams. Designed to be the river in the center of the coverage area, Columbia, Snake, etc.

WATER_OTHER - Covers side rivers, lakes, ponds etc. This coverage is not intended to capture all water outside the main rivers but only water edges that need a breakline and need LiDAR data re-classified. No single line streams are collected.

WATER_ISLAND - Islands in the rivers and streams.

BUILDING - Visible and obvious buildings.

BUILDING_UNSURE - Features that appear to be buildings but might not be.

BUILDING_AREA - Large areas with a dense population of buildings, subdivisions, etc.